

# Investigation of Effect of Boundary Layer on Flow Structure Around a Cylinder with a Strip

Sedat Yayla<sup>1,a</sup> and Süleyman Tekşin<sup>1</sup>

<sup>1</sup> *Department of Mechanical Engineering, Yuzuncu Yil University, 65080 Van, Turkey*

**Abstract.** In this study, the flow characteristic of the circular cylinder was placed vertically in channel which has dimensions as 8000 mm, 1000 mm, 750 mm, length, width and height respectively, was investigated. The cylinder was located in boundary layer with a diameter of 60 mm (D) and a elastic strip which has a 1400 N/mm<sup>2</sup> modulus of elasticity vinyl PVC transparent film was attached behind the cylinder. Length of the strip (L) was 240 mm L/D=4. The Reynolds number was fixed at Re=7500. The time-averaged and instantaneous velocity vector maps, vorticity contours, Reynold shear and normal stresses, turbulent kinetic energy and frequency of shedding were obtained using the particle image velocimetry (PIV) technique. It was found that the elastic plate which exists behind the cylinder has a slight influence on the flow structure of the wake-boundary layer interaction. Values of turbulent kinetic energy, streamwise Reynold stress, transverse Reynold stresses were decreased by attaching strip.

## 1 Introduction

The flow around a cylinder is very important for researchers. Because of that lots of experiments have been done to improve flow structure. Cimbalá and Garg [1] investigated the effect of the attached splitter plate on the flow characteristics downstream of a fixed cylinder and a freely rotating cylinder. The effect of fixed cylinder with an attached plate was similar to the case of a freely rotating cylinder. Zdravkovich & Pridden emphasized the discontinuous jump in base pressure at a critical spacing of the cylinders  $L/D=3.5$ , in which L is the distance between centers of the cylinders and D is the cylinder diameter. [2] Gerrard [3] investigated the effect of length of splitter plate, attached to the circular cylinder, on the wake flow characteristics. He showed that the Strouhal number decreased when the splitter plate length was smaller than the cylinder diameter, but it increased for  $1 < L/D < 2$ . Kwon and Choi [4] conducted a numerical study on the control of vortex shedding in laminar flow downstream of the circular cylinder using splitter plates. They pointed out that the vortex shedding downstream of the circular cylinder completely disappears when the length of the splitter plate is longer than a critical length, which is found to be proportional to the Reynold number. Akilli and Rockwell [5] investigated the vortex formation in the junction of the flat plate and circular cylinder in shallow water flow, using dye visualization and particle image velocimetry (PIV) techniques. Dye visualization showed the formation of counter-clockwise rotating vortices only downstream of the cylinder base, within the wake region. Kwon et al. [6]

investigated the drag reduction caused by ribbons attached to circular cylinders. The position and length of ribbons have a significant effect on the drag reduction. Hwang et al. [7] applied a detached splitter plate for the control of flow induced forces on a circular cylinder in their numerical study of laminar flow. They revealed that optimal location of splitter plate reduces the drag coefficient.

## 2 Experimental set up and instrumentation

Experiments were conducted on a water channel were of 8000 mm × 1000 mm × 750 mm which was made from 15 mm thick transparent Plexiglas sheet with upstream and downstream fiberglass reservoirs. The schematic of experimental arrangement is presented in figure 1. The depth of the water in the test section was adjusted to 600 mm ( $h_w$ ) for the present experiments. The Reynolds number was kept constant as Re=7500. free-stream velocity of 125 mm/s. images were captured at location 250 mm ( $h_m$ ) above the bottom surface of platform.

Velocity vector measurements were performed PIV system equipped by two Nd:Yag pulsed laser sources of a wave length of 532 nm, each with a maximum energy output of 120 mJ. Dantec Flow Map Processor that controlled the timing of the data acquisition was used for synchronizing the camera and laser units. Also CCD camera was used to capture the images with a resolution of 1600 x 1186 pixels. 350 instantaneous images were

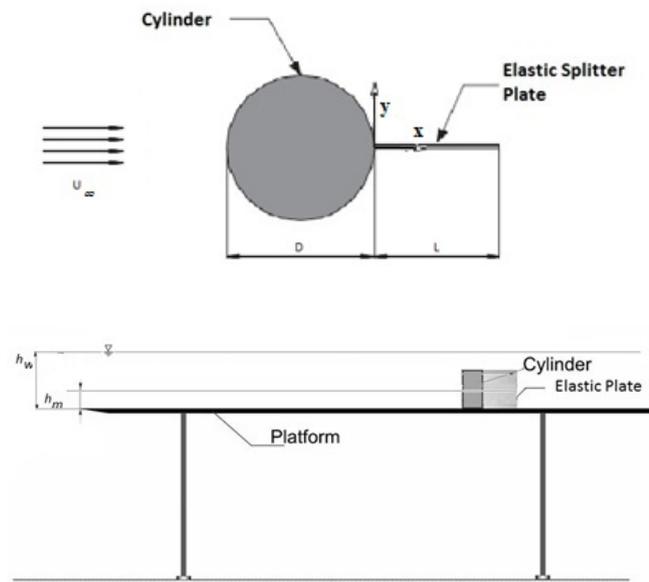
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<sup>a</sup> Corresponding author: [syayla@yyu.edu.tr](mailto:syayla@yyu.edu.tr)

taken with frequency of 15 Hz for each capturing. In the image processing, 32 x 32 pixels with rectangular effective interrogation windows was used. During the process, an overlap of 50% was employed. Totally 7227 (99x73) velocity vectors were obtained (at a rate of 15 frames per second) for an instantaneous velocity field.

The depth of water was maintained at 600 mm as a constant value which implies uniform flow formation in the channel owing to no variation in the flow depth (thus the average flow velocity and no fluctuation surface of the water which affects the flow structure). The Froude number, which is defined as  $Fr = U^2/g h_w$ , based on the water depth was 0.002 that smaller than values of one.

The diameter and height of cylinder 60 mm and 500 mm respectively. Length of the elastic splitter plate were selected 240 mm. Laser sheets were oriented parallel to the bottom surface of the water channel at 250 mm height from bottom surface for images.

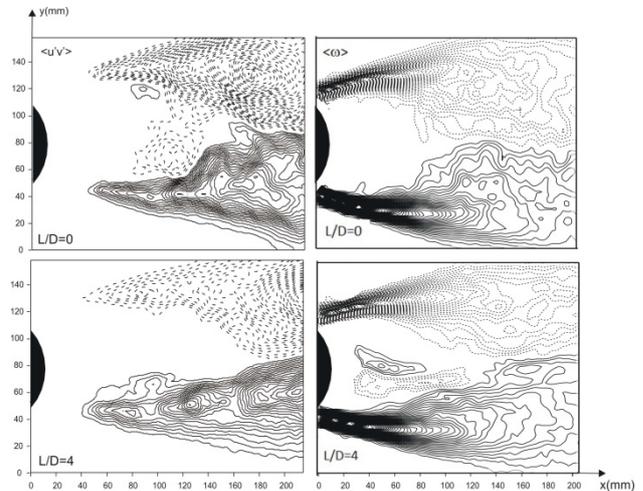


**Figure 1.** Schematic of the experimental system of set-up and definition of the parameters: cylinder diameter  $D$ , length of elastic plate  $L$ , laser sheet height  $h_m$  and free-stream velocity  $U_\infty$ .

### 3 Result and Discussion

Velocity vectors  $V_{avg}$ , streamwise Reynold normal stress  $u'u'/U_{avg}^2$ , transverse Reynold normal stress  $v'v'/U_{avg}^2$ , Reynold stress correlations  $u'v'/U_{avg}^2$ , contours of vorticity  $\omega_{avg}$ , turbulent kinetik energy, are displayed in figures 2-4. Velocity vector fields, in first column, in the second column vorticity, is shown in figure 2. For vorticity contours minimum and incremental values were  $\pm 0.5$  and  $0.5$  respectively. Maximum vorticity values are almost

same for all cases. Foci points and saddle point which are critical location can be seen clearly for both cases. The saddle point is developed for the attached cylinder approximately  $X/D=3.3$ .

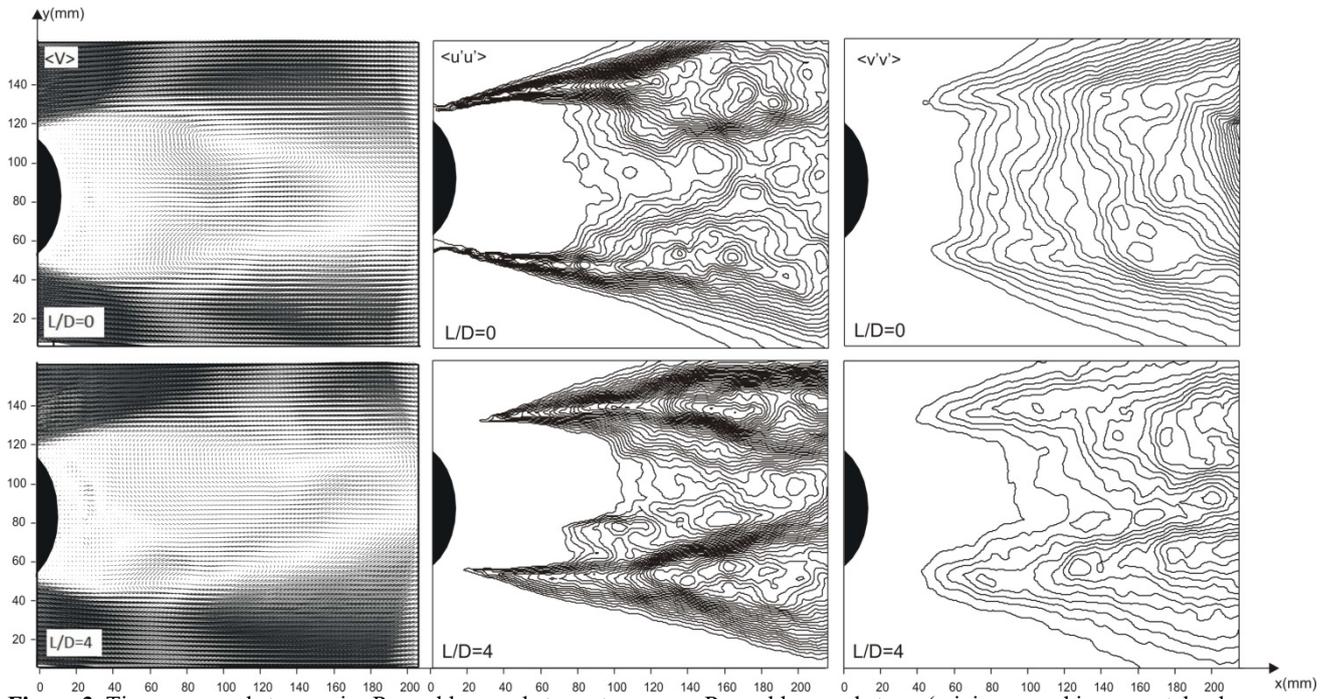


**Figure 2.** Time-averaged Reynolds shear stress and vorticity contours  $\omega_{avg}$  (minimum and incremental values are for Reynold shear stress  $\pm 0.003$  and  $0.003$ . Minimum and incremental values are  $\pm 0.5 \text{ s}^{-1}$  and  $0.5 \text{ s}^{-1}$  for vorticity respectively).

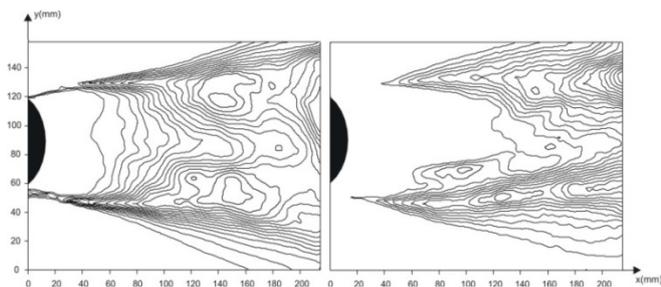
Symmetrical vortex regions can be obtained comparison bare cylinder and with elastic plate attached shape with respect to centerlines of two models.

Maximum values of streamwise Reynold normal stress  $u'u'/U_{avg}^2$ , transverse Reynold normal stress  $v'v'/U_{avg}^2$  and Reynold shear stress correlations  $u'v'/U_{avg}^2$  are shown in figure 3. While the solid lines show the positive (anticlockwise), dashed lines negative (clockwise) spanwise vorticity layers, respectively. For streamwise and transverse Reynold normal stress, minimum and incremental values are  $\pm 0.01$  and  $0.005$  respectively. Reynold shear stress's minimum value is  $\pm 0.003$  and increments are  $\pm 0.003$ . The maximum values of the streamwise Reynold normal stresses of bare and attached body are  $0.21$  and  $0.115$  respectively while transverse Reynold normal stress was decreased from  $0.2$  to  $0.054$ .

Figure 4 shows the contours of the normalized TKE for the two models at  $Re=7500$ . Minimum and incremental values are  $\pm 0.005$  and  $0.01$  respectively. The peak value of the TKE for the bare cylinder has a value of  $0.21$  and that for attached cylinder is  $0.19$  for  $L/D=4$ . For bare and attached body, location of maximum values approximately symmetrical with respect to cylinder centerline. As expected, peak value points were shifted far from the cylinder base.



**Figure 3.** Time-averaged streamwise Reynolds normal stress, transverse Reynolds normal stress (minimum and incremental values are  $\pm 0.01$  and  $0.005$  respectively).



**Figure 4.** Turbulent kinetic energy. Minimum and incremental values are  $0.005$  and  $0.01$  respectively.

## 4 Conclusion

In this study, the passive control of the wake flow past a circular cylinder with at Reynolds number  $7500$  was investigated experimentally using the PIV technique in mechanical engineering department energy division laboratory at Cukurova university. An elastic plate ( $L/D=4$ ) attached behind and center location of the cylinder to control flow around the body. Laser sheet was adjusted at  $250$  mm above the bottom of the cylinder. Images were captured with angle perpendicular to the laser sheet illumination. After capturing images lots of processes were applied to meaningful data. The maximum values of the streamwise Reynolds normal stress with double peaks for the two models occur at locations of approximately  $2.8D$  and  $3D_a$  with values of  $0.21$  and  $0.145$  respectively whereas those of transverse Reynolds normal stress was decreased from  $0.19$  to  $0.09$ .

Data show us that decrease in stress correlations and turbulent kinetic energy for attached bluff body with respect to bare cylinder. In other words, splitter plate which has certain modulus of elasticity can be used to control or suppress the vorticity around the cylinder.

## Nomenclature

$D$	cylinder diameter
$D_a$	attached cylinder
$L$	length of strip
$Re$	Reynolds number
$u$	streamwise velocity component
$v$	transverse velocity component
$U_\infty$	free stream velocity
$\langle \rangle, avg$	average
$u'v'$	Reynolds shear stress correlation
$u'u'$	streamwise Reynolds normal stress
$v'v'$	transverse Reynolds normal stress
$u'$	fluctuations of $u$
$v'$	fluctuations of $v$
$\omega$	vorticity
$V$	velocity vector
$h_w$	height of the water
$h_m$	height of laser sheet

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