

# Error assessment in Image Stereo-correlation

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**Abstract.** The aim of this work is to estimate errors related to Stereo-correlation technique applied to measurements of displacements. In a first step, the influence of the cameras positions is tested using a standard object. In a second step, an evaluation of the stereo-correlation system is achieved. It is based on the generation of synthetic images representative of real speckle patterns deformed. With these images, various parameters are treated in order to determine their impact on the measurement error.

## 1 Introduction

Stereo-correlation is an optical full-field measurement technique which is a mix between Digital Image Correlation (DIC) and stereovision. DIC is an optical full-field measurement technique which was appeared twenty years ago [1, 2, 3]. It consists in recording with a camera some digital images of a specimen undergoing an in-plane displacement field and computing the image correlation by an appropriate software. To characterize the DIC system, systematic studies have been recently proposed by the Workgroup "Metrology" of the French CNRS research network 2519 [4] based on synthetic images undergoing a sinusoidal displacement field. In this paper, we will propose methods which allow the characterization of the stereo-correlation. In the first time, we will determine the error of 3D reconstruction using a standard object. After that, we will adopt the same approach taken by the Workgroup "Metrology" of the French CNRS research network 2519 but adapted to the stereo-correlation technique. We propose a procedure which evaluate errors due to parameters specific to the stereo-correlation with real images (image acquisition, calibration, ...).

## 2 Stereovision

Stereovision is a technique based on the triangulation which calculate the intersection of two projective lines (projection point in the plans of the two CCD sensors), knowing the corresponding one pixel of the first image in the second. Several parameters may affect the accuracy of the measurement. The purpose of this study is to determine the influence of these parameters from the evaluation of the reconstruction error.

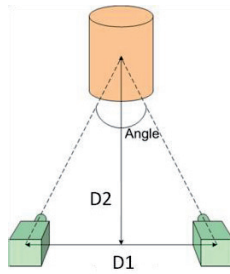
### 2.1 Experimental device

We used a cylinder on which a speckle pattern is bonded. In order to evaluate the influence of the

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camera positions, different configurations were tested: the distance between the two cameras ( $D1$ ) which can be 200, 300 or 400 mm and the distance between the optical centre of the system and the standard object ( $D2$ ) located at 250, 300, 400, 500, 600, 700 or 800 mm. The angle between the two cameras is deduced from these two parameters.



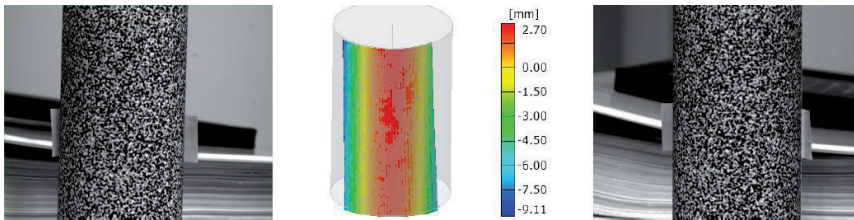
**Fig. 1.** Position parameters of cameras

For each configuration, a theoretical cylinder with a radius 25 mm is fitted by the least squares method on the cloud of measured point. The figure 2 corresponds to the left and right images of the cylinder taken with  $D1=400$  mm and  $D2=700$  mm, and also a 3D reconstruction of the cylinder calculated by stereovision with Aramis 3D software [5]. In order to evaluate the accuracy, systematic, random and RMS error are calculated for each configuration:

$$RMS(X) = \sqrt{\frac{\sum_n (X_{mes} - X_{th})^2}{n}} = \sqrt{\frac{n-1}{n} \sigma^2(X) + \overline{\Delta X}^2} \quad (1)$$

With -  $\sigma(X) = \sqrt{\frac{n \sum_n (X_{mes} - X_{th})^2 - (\sum_n (X_{mes} - X_{th}))^2}{n(n-1)}}$  standard deviation: random error

-  $\overline{\Delta X} = \frac{1}{n} \sum_n (X_{mes} - X_{th})$  average: systematic error



**Fig. 2.** Left and right images and 3D reconstruction of the cylinder with  $D1=400$  mm and  $D2=700$  mm

The RMS error is the measurement error in stereo, this error resulted from different processes (image acquisition, 3D reconstruction, fitting of the perfect cylinder, ...). For each configuration, a theoretical cylinder of radius 25 mm is fitted by the least squares method on the cloud of measured points using a subset size 16 pixels. Then, the error is evaluated using two clouds of points. Indeed, according to the tested configurations, different numbers of points are accessible to measurement. Initially, the cylinder is fitted to all measured points (Figure 3 (a)). In some configurations, the edges of the object are available and lead to increased error. Conversely, in other configurations, only the central part of the object is evaluated. We get a low error because it is an area easier to match. By choosing an identical area  $ZI$  (10x10mm) corresponding to a cloud of points available in all configurations, we obtain additional information which allows comparison between the configurations (Figure 3 (b)).

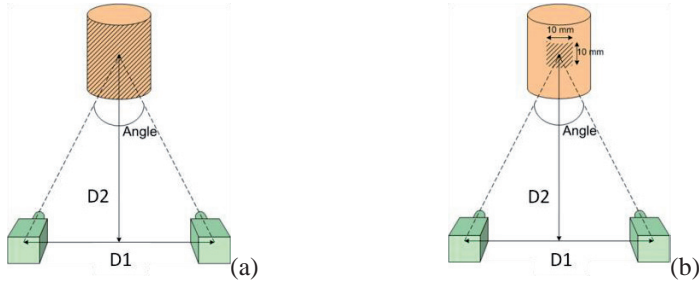


Fig. 3. Position parameters of camera

### 2.2 Results

The distribution of RMS error, the standard deviation and the average as a function of the distance between the two cameras, the distance between the optical centre of the system and the standard object and the angle between the cameras for a subset size of 16 pixels is shown in the Figure 4. The distributions (a) (b) (c) of Figure 4 are obtained with all the points while the distributions (d) (e) (f) of Figure 4 are made from the points of the zone *ZI*. According to the measured area, the distribution is different but in both cases the RMS error is controlled by the standard deviation, the systematic error is low. We note that the maximum RMS error (0.0226 mm) is reached for  $D1=200\text{mm}$  and  $D2=500\text{mm}$  (ie angle =  $22.6^\circ$ ) in the case of adjustment on all measured points when he reached 0.0084 mm *ZI*. In this zone *ZI*, each configuration leads to statistics based on the same sample. We find that the more we move away from the object, the more the RMS error increases. The study on all measured points leads statistics based on variable samples, larger samples when the angle between cameras is small, a small angle (less than  $30^\circ$ ) produces a larger RMS errors.

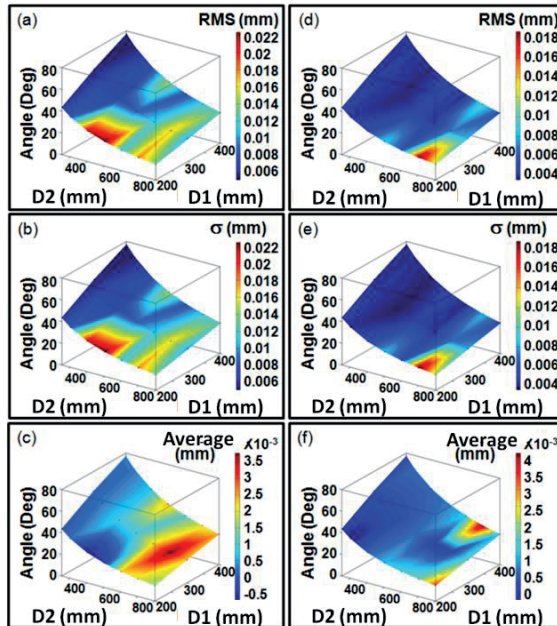
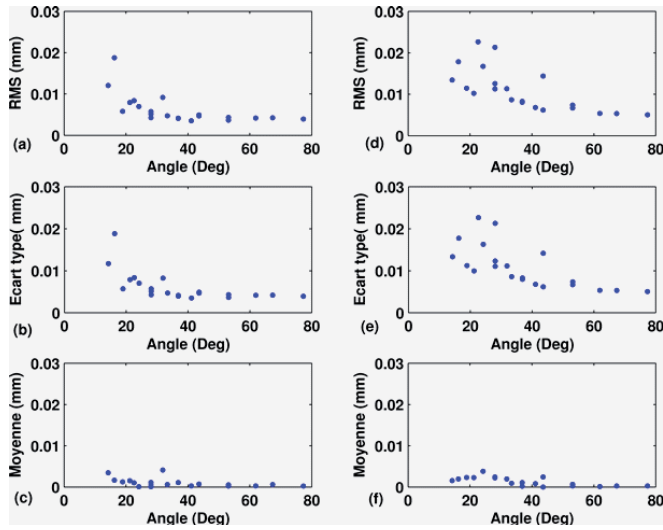


Fig. 4. RMS error, standard deviation and average as a function of  $D1$ ,  $D2$  and angle for the total area (a) (b) (c) and with *ZI* (d) (e) (f)



**Fig. 5.** RMS error, standard deviation and average as a function of the angle with ZI (a) (b) (c) and for the total area (d) (e) (f)

The graphs in Figure 5 show the influence of the angle between the cameras on the reconstruction error. Whatever the points used (distributions (a) (b) (c) from the points of the zone Z1 and distributions (d) (e) (f) with all points); we note that when we increase the angle between the cameras, we can observe two phenomena: a reduction of RMS error and a decrease of the dispersion of RMS errors. This dispersion is noticeable from an angle of  $50^\circ$  and is increasing with the decrease of angle, especially when we use all points of measurement. Dispersion is important in the case of fitted by the least squares method on the 25mm radius from an angle of  $30^\circ$ . The best reconstructions were performed with an angle greater than or equal to  $30^\circ$ , the RMS error obtained is less than 0.01 mm on all points and 0,005 mm with Z1. With a large angle, the vision field will be reduced. The compromise is therefore  $30^\circ$ .

### 3 Stereo-correlation

The techniques of digital image correlation and reconstruction were evaluated separately, the first in many studies encountered in the bibliography [4, 6, 7, 8, 9, 10], the second in the previous section. To test the DIC part and the reconstruction part simultaneously, we wanted to conduct a study similar to the work of the Workgroup “Metrology” of the French CNRS research network 2519 [4]. The idea is to use perfect synthetic images that we can control some parameters (speckle size, deformation, ...). A computation made by a software of stereo-correlation requires a pair of images from two different cameras and a calibration to determine the positions of the cameras. Two solutions are possible. With our equipment, we are unable to conduct a study in stereo-correlation with synthetic images. We have therefore decided to conduct a study with real images from the synthetic images.

#### 3.1 Experimental device

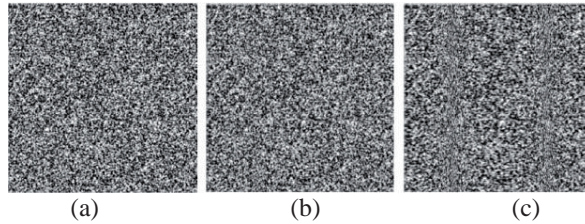
As for the work of the Workgroup “Metrology” of the French CNRS research network 2519 [4] previously discussed, the sets of synthetic speckle-pattern images are obtained using the TexGen software [11] which produces synthetic 8-bit speckle-pattern images as realistic as possible to DIC speckle patterns. The set of deformed images are obtained assuming only an unidirectional sinusoidal displacement which is given by:

$$\underline{U}(x) = \alpha \cdot p \cdot \sin\left(\frac{2\pi x}{p}\right) \underline{e}_x \quad (2)$$

$$\underline{U}_x(x) = \frac{\partial U}{\partial x} = 2\pi\alpha \cdot \cos\left(\frac{2\pi x}{p}\right) \underline{e}_x = U_{,x}^{Max} \cos\left(\frac{2\pi x}{p}\right) \underline{e}_x \quad (3)$$

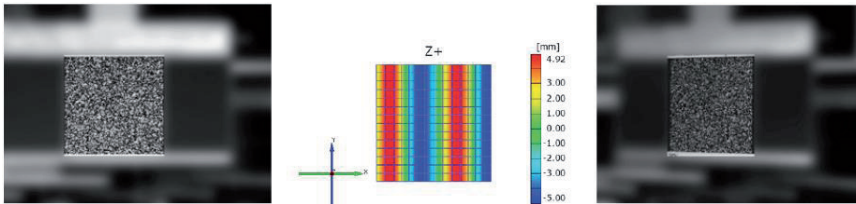
$$\underline{U}_{,xx}(x) = \frac{\partial^2 U}{\partial x^2} = \frac{-4\pi^2\alpha}{p} \cdot \sin\left(\frac{2\pi x}{p}\right) \underline{e}_x = -U_{,xx}^{Max} \sin\left(\frac{2\pi x}{p}\right) \underline{e}_x \quad (4)$$

where  $p$  is the period in pixel and  $\alpha p$  the amplitude of deformation. Chosen values for the strain amplitude  $\alpha$  and for the period  $p$  are respectively  $\alpha \in \{0.02; 0.01; 0.005; 0.001\}$  and  $p \in \{10; 20; 30; 60; 130; 260; 510\}$  pixels, for 512x512 pixel images. Note that corresponding values of the maximum displacement gradient are 12.6%, 6.3%, 3.1% and 0.6%, respectively.



**Fig. 6.** Example of simulated synthetic images: reference (a) and deformed images ( $p = 260$  pixels, (b)  $\alpha=0.02$ , (c)  $\alpha=0.1$ ).

The use of real images for this study produces some errors. We can mention errors due to non perfect cameras (calibration, distortion, sharpness, ...), the environment (difference in contrast between images, ...) or the test itself. To minimize errors due to the test, we used synthetic images. This choice allows us to control the deformation very precisely. To avoid any rigid body movement during image changes, and then add errors to the correction of these movements, the synthetic images described earlier scrolled on a computer screen (LCD, 1920x1200 pixels) .

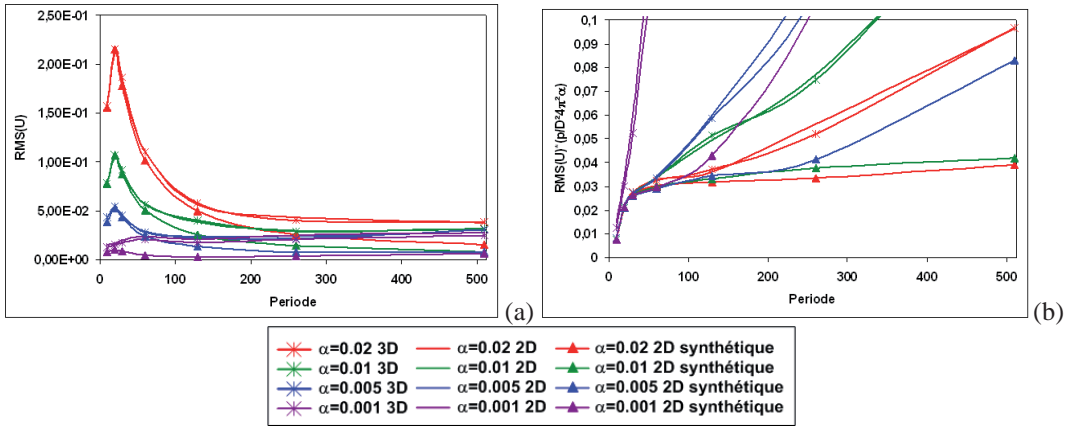


**Fig. 7.** Left and right images and the x displacement field

The left camera is placed parallel to the plane of the screen to use images taken by this camera in digital image correlation. As for the previous study, the results are presented in terms of systematic, random and RMS error.

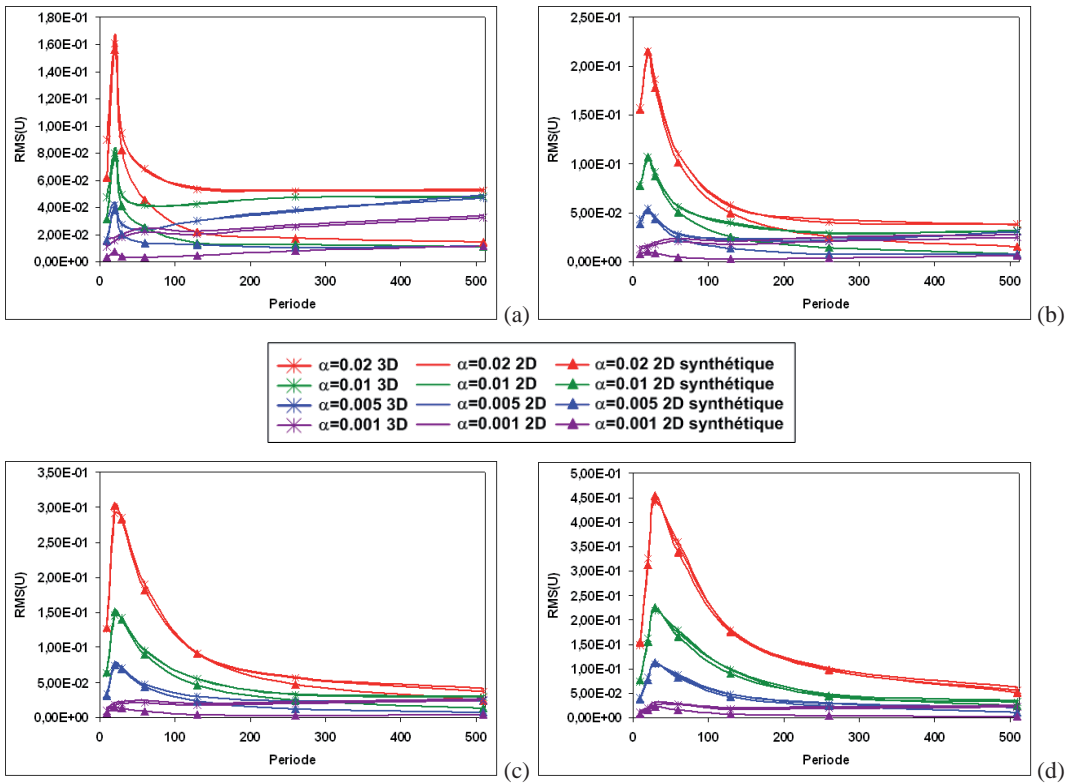
### 3.2 Results

Figure 8 shows the RMS and the RMS divided by the maximum second derivative of the displacement and  $D^2$  as a function of period  $p$  for stereo-correlation and DIC with real images and DIC with synthetic images with a subset size  $D=16$  pixels. It has been shown in [4] that these curves for digital image correlation can be analyzed considering three zones. In the first one for small periods (typically for  $p \leq D$ ), the software evaluate nothing else than the standard deviation of the displacement itself. When the period is greater than about  $5D$ , an asymptotic value can be reached. This asymptotic value is essentially controlled by the second gradient : it increases as the second gradient increases. The second zone is the transition zone between the other two. However, it has been shown that for small strains, asymptotic value is not reached and the error is controlled by others parameters (see [4] for details).



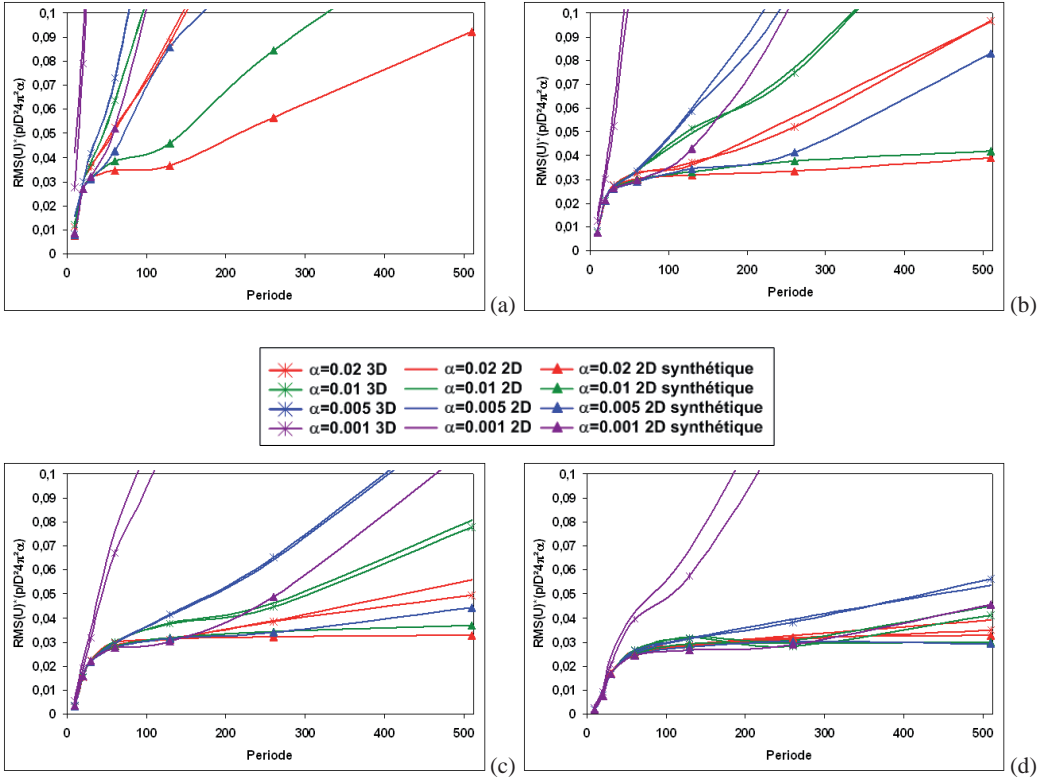
**Fig. 8.**  $RMS(U)$  (a) and  $RMS(U)/D^2 U^{Max}_{xx}$  (b) as a function of period  $p$  for various strain amplitudes  $\alpha$  and a subset size  $D=16$  pixels

The curves of  $RMS(U)$  as a function of period  $p$  show that the transition between the stereo-correlation and DIC with real images has little influence in our case. Indeed the curves for these two configurations are very close with still better performance for stereo-correlation. This trend can be explained by a misalignment of the left camera used for correlation.



**Fig. 9.**  $RMS(U)$  as a function of period  $p$  for various strain amplitudes  $\alpha$  and a subset size  $D=10$  pixels (a),  $D=16$  pixels (a),  $D=22$  pixels (a),  $D=32$  pixels (a).

Furthermore, when we compare the results with real images and results with synthetic images, we find that the bias associated with the acquisition of images is not negligible and supplants the error due the stereovision. Another source of errors due to the acquisition may be linked to the images themselves. Indeed, to capture the synthetic images through the cameras, we have scrolls on a computer screen. The refresh rate of screen, the resolution, the scaling of images are parameters that may affect the measurement and could explain the differences between curves.



**Fig. 10.**  $RMS(U)/D^2U^{Max}_{,xx}$  as a function of period  $p$  for various strain amplitudes  $\alpha$  and a subset size  $D=10$  pixels (a),  $D=16$  pixels (a),  $D=22$  pixels (a),  $D=32$  pixels (a).

To test the influence of the subset size, the 28 previous images have been used with 4 subset size  $D$  10, 16, 22 and 32 pixels. The graphs of Figures 9 and 10 representing the RMS (U) and the ratio  $RMS(U)/D^2U^{Max}_{,xx}$  as a function of period  $p$ , reveal an influence of the subset size on the displacement errors. We find the different regimes described above with a increasing divergence of the curves of the  $RMS(U)/D^2U^{Max}_{,xx}$  for low strain amplitudes  $\alpha$ . The asymptote is reached only for large subset sizes.

## 4 Conclusion

To test the stereovision and DIC systems independently, we captured images of a standard object, and by fitting by the least squares method of a perfect cylinder on the cloud of measured point, the reconstruction error could be determined. The results obtained with different configurations of the stereovision sensor have highlighted the influence of parameters related to the sensor (distance between cameras, the optical centre of the system and the standard object, angle between the cameras).

By creating well controlled synthetic images, we are able to estimate errors related to Image Stereo-correlation technique applied to measurements of displacements. With deformed images obtained assuming only a unidirectional sinusoidal displacement with different values for the amplitude and the period, we checked relationship between parameters associated with the displacement (amplitude and gradient) for the stereo-correlation.

## References

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