Centre of Excellence for Nuclear Materials

Workshop

Materials Innovation for Nuclear Optimized Systems

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Steven J. ZINKLE
Oak Ridge National Laboratory (USA)

Opportunities and Challenges for Materials Innovation in Nuclear Energy

Workshop organized by:
Christophe GALLÉ, CEA/MINOS, Saclay – christophe.galle@cea.fr
Constantin MEIS, CEA/INSTN, Saclay – constantin.meis@cea.fr

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Opportunities and Challenges for Materials Innovation in Nuclear Energy

Steven J. ZINKLE

Oak Ridge National Laboratory (Oak Ridge, Tennessee, USA)

Materials performance is central to the satisfactory operation of current and future nuclear energy systems. For example, the remarkable improvement in the operation and reliability of Generation-II light water reactors (LWRs) over the past 25 years has been largely associated with improvements in steam generator materials, fuel cladding technology (composition and fabrication), and improved understanding of water chemistry impacts on corrosion and deposition. Future fission and proposed fusion energy systems will be increasingly dependent on advanced structural materials to reliably deliver high performance with favorable safety attributes and acceptable economic cost. In many cases, the proposed operating temperatures are significantly higher than the experience base for light water reactors. This motivates development of structural materials with improved high temperature strength for prolonged operating periods and engineered corrosion resistance for the candidate coolants and other materials in the system. The high radiation fluxes in future nuclear energy systems will require the structural materials to have superior radiation resistance compared to currently available materials. The material performance demands are particularly challenging for the fuel cladding and wrapper of next-generation sodium-cooled fast reactors, where simultaneous resistance to high temperature thermal creep and radiation-induced property degradation up to doses of \(\sim 100-150\) dpa is required.

Several strategies can be utilized to develop structural materials with simultaneous high radiation resistance, high strength, good toughness and corrosion resistance, and moderate fabrication cost. There are three general approaches for designing radiation resistance: Nanoscale precipitates or interfaces to produce high point defect sink strength (e.g., oxide dispersion strengthened (ODS) and next-generation ferritic/martensitic steels with high particle densities); purposeful utilization of immobile vacancies (e.g., SiC/SiC ceramic composites); and utilization of radiation-resilient matrix phases (e.g., ferritic instead of austenitic steel matrix, etc.). High-performance steels designed using computational thermodynamics are demonstrating promising capability to produce a high density of highly stable nanoscale precipitates that could serve as efficient point defect recombination centers during irradiation, and also provide good thermal creep strength at high temperatures [1]. Figure 1 shows an example of improvements in high temperature thermal creep properties for a 9%Cr-1%Mo ferritic martensitic steel that was achieved simply by slightly altering the thermomechanical processing procedure. Figure 2 compares the fracture toughness behavior of an advanced ODS ferritic steel before and after low dose neutron irradiation at 300°C [2]. The ductile to brittle transition temperature (DBTT) in the LT orientation remained below -150°C with a shift in the DBTT of about 12°C; the corresponding shift in the DBTT for EUROFER97 (9Cr-2WVTa) ferritic/martensitic steel was about 39°C. Higher dose studies are in progress.

It will be important for nuclear energy researchers to continue to closely interact with the broader materials science and engineering community in order to effectively leverage innovations that continue to occur in the broad field of materials science. For example, practical aspects used in the aerospace industry to reduce the time from invention of a new alloy system to code qualification and commercialization could be useful for development of new structural materials for nuclear energy systems. In the future, utilization of emerging advanced manufacturing processes such as additive manufacturing to produce near-net shape parts with precise microstructural control will be of increasing importance to control fabrication costs and to create high-performance fabrication architectures that could not be achieved using conventional fabrication methods.
Following the accident at the Fukushima Daiichi site in Japan, there is increasing interest in exploring accident tolerant or enhanced safety margin fuel systems for existing and future reactors, which could potentially provide increased response time or reduced consequences via reduced enthalpy production, reduced hydrogen production, and delayed clad rupture or fission product release during a loss of coolant accident compared to conventional Zr alloy cladding/monolithic UO₂ fuel systems. Although all alternative fuel systems have technological or neutronic shortcomings, exploratory research would be useful to quantify their potential improved accident tolerance so that an informed decision on the best option(s) for future LWR fuel systems can be reached. If research results on a particular accident tolerant concept prove to be promising, it might be possible to initiate confirmatory tests in commercial reactors within about 10 years.

Fig. 1: Comparison of creep rupture behavior of 9%Cr steels at 650°C after conventional and new thermomechanical treatment [1].

Fig. 2 : Comparison of the fracture toughness of 14YWT ODS ferritic steel before and after neutron irradiation to 1.5 dpa at 300°C [2].

References

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Nuclear Energy

Steven J. Zinkle
Oak Ridge National Laboratory
Oak Ridge, Tennessee, USA

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Overview of Challenges and Opportunities

• Many commercial alloys are operating near their performance limits and exhibit variable heat-to-heat performance
  – Artifacts of empirical/evolutionary approach to developing new alloys

• Future goals for nuclear energy involve even more extreme operating environments
  – Plant life extensions for LWRs
  – Gen IV fission and fusion reactors (higher doses and temperatures)

• The accident at the Fukushima Dai-ichi power plant is causing some nations to reconsider the future of nuclear energy

• Recent results suggest combination of new tools such as computational thermodynamics and knowledge of degradation mechanisms (creep-fatigue, radiation effects, etc.) can be used to design very high-performance materials
Comparison of Gen IV and Fusion Structural Materials Environments

All Gen IV and Fusion concepts pose severe materials challenges
Heat to Heat Variability has been a Common Feature of Structural Alloys

Alloy 617 Thermal Creep

Heat 1

Heat 2

Heat 3

13.5 N-mm\(^{-2}\) helium

P.J. Ennis et al. 1984
Today We Know That Very Long Time Service Causes The Properties of 9Cr-1MoVNb to Decrease to a Greater Extent Than Anticipated In Initial Alloy Design.

Exposure of 9Cr-1MoVNb Tubing for 155,000 h at 550-590°C Produces Laves Phase Precipitation and Substructure Recovery.

The Tensile Strength of 9Cr-1MoVNb Decreased 15% As A Result Of Long-Time Steam Boiler Tubing Service.

Computational thermodynamics: ~6.3% of ASME allowable compositions for grade 92 produced ferrite at the 1040°C normalizing temperature (Vitek & Santella, ORNL)

Results were consistent with expectations based on aging studies of Brinkman (ORNL) in 1990.
Radiation Damage can Produce Large Changes in Structural Materials

- Radiation hardening and embrittlement (<0.4 $T_M$, >0.1 dpa)

- Phase instabilities from radiation-induced precipitation (0.3-0.6 $T_M$, >10 dpa)

- Irradiation creep (<0.45 $T_M$, >10 dpa)

- Volumetric swelling from void formation (0.3-0.6 $T_M$, >10 dpa)

- High temperature He embrittlement (>$0.5 T_M$, >10 dpa)

Examples of radiation damage degradation in steels

**Fracture toughness of Types 304 and 316 stainless steel irradiated at 250-350°C**

<table>
<thead>
<tr>
<th>Steel Type</th>
<th>Fracture Toughness $K_I$ (MPa-m$^{1/2}$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>316LN Pawel</td>
<td>300-400</td>
</tr>
<tr>
<td>316Ti Rodchenkov</td>
<td>250-350</td>
</tr>
<tr>
<td>316LN Rodchenkov</td>
<td>200-300</td>
</tr>
<tr>
<td>316LN van Osch</td>
<td>150-250</td>
</tr>
<tr>
<td>316 odette lucas</td>
<td>100-200</td>
</tr>
<tr>
<td>316 odette lucas</td>
<td>50-150</td>
</tr>
<tr>
<td>316SS odette lucas</td>
<td>0-100</td>
</tr>
<tr>
<td>304 Mills 1997</td>
<td>400-500</td>
</tr>
<tr>
<td>316 Mills 1997</td>
<td>350-450</td>
</tr>
<tr>
<td>304/316L Ehrmsen Chopra</td>
<td>300-400</td>
</tr>
<tr>
<td>304/316L CR-G960 Chopra</td>
<td>250-350</td>
</tr>
<tr>
<td>304/304L Denna Chopra</td>
<td>200-300</td>
</tr>
<tr>
<td>304/304L MRP Chopra</td>
<td>150-250</td>
</tr>
<tr>
<td>304 JAPEI(GT) Chopra</td>
<td>100-200</td>
</tr>
<tr>
<td>304 JAPEIC(SR) Chopra</td>
<td>50-150</td>
</tr>
<tr>
<td>304 JAPEIC(BB) Chopra</td>
<td>0-100</td>
</tr>
</tbody>
</table>

**Comparison of Volumetric Swelling in Fast Fission Reactor Irradiated Austenitic and Ferritic-Martensitic Steels**

- Contribution to SCC in LWR internals
- Conventional stainless steels are not attractive options for high dose Gen IV reactor applications

*Zinkle & Was, Acta Mater. 61, in press (diamond jubilee special issue, 2013)*
Cavity swelling in neutron-irradiated 8-9%Cr reduced activation ferritic-martensitic steels may become significant for fusion-relevant He/dpa values

He mainly produced at start of irradiation

Effect of Neutron Irradiation on the Ductile to Brittle Transition Temperature of Reduced Activation 9Cr Ferritic/Martensitic Steels

Can we break the shackles that limit conventional structural materials to ~300°C temperature window?

Structural Material Operating Temperature Windows: 10-50 dpa

Additional considerations such as He embrittlement and chemical compatibility may impose further restrictions on operating window.

\[ \eta_{\text{Carnot}} = 1 - \frac{T_{\text{reject}}}{T_{\text{high}}} \]


Approaches for radiation resistance 1: High sink strength

- High density of nanoscale precipitates or particles (e.g., ODS steel or Ti-modified austenitic stainless steel)

High density of stable precipitates can also improve thermal creep strength

- High density of interfaces (grain boundaries or multilayers)


Misra, Hoagland, Demkowicz, etc.
Effect of Initial Sink Strength on the Radiation Hardening of Ferritic/martensitic Steels

Approaches for radiation resistance 2: Immobile defects

- Defect accumulation is limited if one or more defect types are immobile
  - Utilize materials with negligible point defect mobility at desired operating temperatures
  - A key potential consequence (particularly in ordered alloys and ceramics) is amorphization, with accompanying significant volumetric and property changes

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Regime with intrinsically high point defect recombination typically occurs at too low of temperatures for power generation applications (except SiC and possibly Al₂O₃, W, Re)

*after S.J. Zinkle, Chpt. 3 in Comprehensive Nuclear Materials (Elsevier, 2012)*
Irradiation-induced swelling in SiC

![Graph showing irradiation-induced swelling in SiC](image)

- **Amorphous Regime**
- **Saturable Regime**
- **Non-Saturable Regime**

- **Snead 2006**
- **Price 1973**
- **Blackstone 1971**
- **Price 1969**
- **Snead, Unpub.**

- **800°C, 40 dpa**
- **8.5 dpa**
- **5 dpa**
- **1.75 dpa**

- **Stage I**
- **Stage III**

**Irradiation Temperature (°C)**

**Swelling (%)**

Managed by UT-Battelle for the U.S. Department of Energy
Approaches for radiation resistance 3: Utilize matrix phases that are resistant to defect accumulation (e.g., BCC or noncrystalline phases)

MD: Large vacancy clusters are not directly formed in BCC metal displacement cascades

Void swelling in Fe is significantly less than in Cu for the same dose
Defect accumulation is lower in BCC steels compared to FCC

Comparison of defect cluster formation in neutron irradiated austenitic and ferritic stainless steel (0.065 dpa, 120°C)

Type 308 stainless steel weld metal

\[ \text{δ-ferrite} \]

\[ N=2 \times 10^{21} / m^3 \]

\[ d=5.2 \text{ nm} \]

100x lower density

\[ \text{Austenite} \]

\[ N=6 \times 10^{23} / m^3 \]

\[ d=1.66 \text{ nm} \]

S.J. Zinkle & R.L. Sindelar, unpublished
Modern steels exhibit reduced hardening and less embrittlement compared to 1960s-era RPV steel

Hardening rate of 9Cr steels is about 50% that of RPV steels

Embrittlement rate of 9Cr steels is about 40% that of RPV steels (normalized to same amount of radiation hardening)

Plotted data are 8-9%Cr steels; similar results obtained for pressure vessel-relevant steels such as modern 2-3%Cr steels

Rensman, Lucon, SCK-CEN
Sokolov, ASTM STP 1325
M.A. Sokolov et al., J. Nucl. Mater. 367-370 (2007) 68
New reduced activation steels designed with computational thermodynamics exhibit superior mechanical properties compared to conventional steel

- Three experimental 9Cr RAFM heats (1537, 1538, 1539), together with an optimized-Gr.92 heat (C3=mod-NF616), were investigated
  - composition changed to favor MX and reduce Laves phase, M23C6, and Z-phase
- Tensile strength of new TMT steels were much higher than conventional steels
- Dramatic improvement in thermal creep strength also observed

1.6X
Comparison of thermal creep strengths of current and compositionally modified ferritic/martensitic steels

Modified 9Cr-1Mo—New TMT

(modified by D. Stork, Culham, to include recent Tata Steels data)
Creep Resistance of the Advanced 9Cr FM Steels

- Relative to Gr92, all the advanced 9Cr FM steels showed enhanced creep resistance; Gr92-2b (TMT) and Ti-modified alloys were best.
  - The amount of MX-type nano-precipitates increased with thermal aging, which favored the enhancement of creep resistance.

Fine-scale precipitates also provide high point defect sink strength.
Comprehensive Property Assessment of Advanced Austenitic Alloys for Sodium-cooled Fast Reactor (SFR)

- Newly developed alloy based on HT-UPS (Fe-14Cr-16Ni base) exhibited:
  - Improved weldability compared to the original HT-UPS.
  - Moderate creep resistance when 10\% cold-work applied (much better than 316H, comparable to NF709).
  - Thermal stability/creep-fatigue properties of new alloys were not as good as NF709.

- Current US focus is evaluation of NF709 (Fe-22Cr-25Ni base).
Computational Thermodynamics Sped Development of Alumina-Forming Austenitic (AFA) Stainless Steels

- AFA: Order of magnitude better corrosion resistance with excellent creep resistance and low alloy cost
- Initial findings published in *Science*, April 20, 2007
- 2009 R&D 100 Award Winner
Proof of Principle Established For Design of Creep Resistant Cast Forms of NbC-Strengthened Alumina-Forming Austenitic (AFA) Steel

- Nb, Si, C contents co-optimized for alumina formation, creep resistance and casting (vacuum arc-cast): Fe-25Ni-14Cr-3.5Al-1Nb base - high C castings have better creep resistance than wrought AFA - promising oxidation resistance up to 700-800°C (more data and further optimization needed)

- Next step is trial air castings of promising compositions
Low-Cost, Alumina-Forming, Fe-Base Superalloy

DARPA Funded Next Generation Alumina-Forming Austenitic (AFA) Stainless Steel Targeting 10x Better Creep Resistance

Move from Carbide to $\gamma'$-Ni$_3$Al Strengthening

Thermodynamic Calculation of Candidate Alloy Creep-Rupture Life Behavior (700°C/170MPa)

- ORNL AFA stainless steels: 2009 R&D 100 Award, licensed to Carpenter Tech. 2011
  - Superior high-temperature corrosion resistance over stainless steels (Al$_2$O$_3$ surface)
  - Carbide precipitates provide creep resistance comparable to advanced stainless steels

- DARPA funded discovery of $\gamma'$-Ni$_3$Al strengthened AFA w/greatly improved creep resistance while retaining ability to form Al$_2$O$_3$ for superior corrosion resistance
New 12YWT Nanocomposited Ferritic Steel has Superior Strength compared to conventional ODS steels

- Thermal creep time to failure is increased by several orders of magnitude at 800°C compared to ferritic/martensitic steels
  - 2% deformation after ~2 years at 800°C, 140MPa
- Potential for increasing the upper operating temperature of iron based alloys by ~200°C
- Acceptable fracture toughness near room temperature


- Atom Probe reveals nanoscale clusters to be source of superior strength
  - Enriched in O(24 at%), Ti(20%), Y (9%)
  - Size : \( r_g = 2.0 \pm 0.8 \text{ nm} \)
  - Number Density : \( n_v = 1.4 \times 10^{24}/\text{m}^3 \)
- Original \( \gamma_2 \text{O}_3 \) particles convert to thermally stable nanoscale (Ti,Y,Cr,O) particles during processing
- Nanoclusters not present in ODS Fe-13Cr + 0.25\( \gamma_2 \text{O}_3 \) alloy
Recent research suggests high-strength steels that retain high-toughness are achievable

- Generally obtained by producing high density of nanoscale precipitates and elimination of coarse particles that serve as stress concentrator points

![Graph showing the relationship between fracture toughness and ultimate tensile strength for different steels.](image)

**Graph Description**

- **1st and 2nd generation steels** (HT9, 2 1/4Cr-1Mo, etc.)

- **Ultra high strength steels** (nanocomposited ODS, Aermet, etc.)

- **14YWT ODS steel**

The magnitude of low temperature radiation embrittlement can be suppressed by using a very high concentration of radiation defect sinks.

300°C, 1.5dpa: Minimal DBTT shift in 14YWT, vs. 85°C shift for Eurofer ODS steel.
Advanced Manufacturing Techniques offer the potential to enable rapid fabrication of complex geometries

Examples of additive manufacturing technologies

<table>
<thead>
<tr>
<th>Electron beam melting</th>
<th>Ultrasonic additive manufacturing</th>
<th>Laser metal deposition</th>
<th>Fused deposition modeling</th>
</tr>
</thead>
<tbody>
<tr>
<td>• Precision melting of powder materials</td>
<td>• Simultaneous additive and subtractive process for manufacturing complex geometries</td>
<td>• Site-specific material addition</td>
<td>• Precision deposition of thermoplastic materials</td>
</tr>
<tr>
<td>• Processing of complex geometries not possible through machining</td>
<td>• Solid-state process allows embedding of optical fibers and sensors</td>
<td>• Application of advanced coating materials for corrosion and wear resistance</td>
<td>• Development of high-strength composite materials for industrial applications</td>
</tr>
<tr>
<td></td>
<td></td>
<td>• Repair of dies, punches, turbines, etc.</td>
<td>• Transformation of rapid prototyping to rapid manufacturing</td>
</tr>
</tbody>
</table>
Overview of SiC/SiC composites for nuclear energy

- Fission reactor irradiation stability up to 40 dpa confirmed for current-generation SiC/SiC composites
- Outstanding issues include improvements in leak-tightness and fabrication (complexity and cost) and development of structural design criteria

Data from recent US/J HFIR study
Status and recent highlights: SiC/SiC composites

- Fission reactor irradiation stability up to 70 dpa at 500 and 800°C
  - Further improvements in development of stoichiometric SiC fibers may be needed for higher dose applications
- Scoping low dose irradiation studies on SiC joints found no degradation for several joining technologies

Hi-Nicalon Type S fiber reinforced CVI SiC

70 dpa at 300-800°C

Y. Katoh et al., ORNL/TM-2012/459 (2012)

Y. Katoh et al., NuMat, Osaka, Japan (2012)
US Reactor Fuel Performance: Higher burnup with fewer failures

Fuel Performance History for US Light Water Reactors

Zinkle & Was, Acta Mater. 61, in press (diamond jubilee special issue, 2013)
There are three major potential strategies for accident tolerance:

- **Improved Fuel Properties**
  - Lower operating temperatures
  - Clad internal oxidation
  - Fuel relocation / dispersion
  - Enhanced retention of fission products
  - Fuel melting safety margin

- **Improved Cladding Properties**
  - High temperature clad strength and fracture
  - Thermal shock resistance
  - Resistance to melting
  - Resistance to hydrogen embrittlement

- **Suppressed Reaction Kinetics with Steam**
  - To minimize enthalpy input and hydrogen generation
    - Oxidation rate
    - Heat of oxidation

**Potential options for fuel cladding include:**
- Oxidation-resistant alloy cladding (e.g., steels)
- Oxidation-resistant coatings on Zr alloy cladding
- Ceramic matrix composite cladding
A Loss of Coolant Accident (LOCA) such as what occurred at the Fukushima Dai-ichi site is the most severe postulated safety case for nuclear reactors

- Loss of offsite power due to tsunami 1 h after reactor scram
  - On-site diesel generators and battery power was lost immediately (unit 1) or after a few days (units 2&3)
  - Inability to remove MWs of residual heat led to temperature increase in the core
- At high temperatures, the Zr alloy cladding oxidation increases and becomes the dominant source of heat (with H$_2$ gas as a byproduct)
Oxidation behavior of zircaloy cladding under LOCA conditions

Cladding temperature evolution (600°C steam) for different cooling periods

K. Terrani, L. Snead, S. Zinkle et al., to be published
Thermal creep strength of some candidate cladding materials

Comparison of 100 h creep rupture strengths of candidate fuel cladding materials

- Mo alloys and steels (and SiC/SiC, not plotted) offer improved high temperature strength
High-Pressure Steam Oxidation Tests:
Comparison of the Extent of Steam Reaction

Various materials exposed to pure steam for 8 hours (various flow rates and pressures):
- Zircaloy: Pawel-Cathcart and Moalem-Olander data
- 317 Stainless Steel: ORNL high-pressure tests; thickness loss data
- NITE and CVD SiC: ORNL high-pressure tests; thickness loss data
- 310 Stainless Steel: ORNL high-pressure tests; mass gain data converted to thickness loss
- FeCrAl Ferritic Steel: ORNL high-pressure tests; mass gain data converted to thickness loss

![Graph showing material recession vs. temperature for different materials.](image-url)
Comparison of Advanced Fe-based Alloys Steam Oxidation Rate with Zr Alloys

Temperature [°C]

Parabolic Oxidation Rate Constant

$k_{ox} [g/cm^2 \cdot s^{1/2}]$

Zirconium Alloys
- Baker-Just
- Leistikow-Schanz
- Urbanic-Heidrick
- Pawel-Cathcart
- Moalem-Olander
- Zry-4
- Duplex
- Zirlo
- M5
- E110

Iron Alloys
- 304SS - Ishida et al.
- 304SS - Brassfield et al.
- 310SS - Pint et al.
- FeCrAl

2 - 3 Orders of Magnitude Reduction in Oxidation Kinetics
Neutronics and Economics of Steel Clad

Two strategies to make up for higher neutron absorption in the steel cladding and maintain identical cycle lengths to Zr clad:

- Reduce clad thickness (steel is stronger and more oxidation resistant)
- Increase $^{235}\text{U}$ enrichment

$^{235}\text{U}$ Enrichment [%] vs Cladding Thickness [µm]

Results in 15-25% Increase in Fuel Cost

K. Terrani, L. Snead, S. Zinkle et al., to be published

Difference In End Of Life Reactivity SS Clad Vs Zr Clad
Several Accident Tolerant Fuel Concepts are Under Consideration, including:

- **UO$_2$ – Zircaloy** (Base Case)

- **UO$_2$ – FeCrAl** (oxidation resistant Steel)

- **FCM – FeCrAl**
  Fully Ceramic Microencapsulated Fuel

Improved oxidation-resistant Zr cladding (coatings or alloys) is also being considered.
Conclusions

• A high density of nanoscale dispersoids in ferritic/martensitic and austenitic steels is a promising approach to simultaneously achieve improved radiation resistance and high temperature strength
  – Ultrahigh densities approaching $10^{24}/m^3$ may provide dramatic improvements

• Computational thermodynamics is a convenient tool for rapidly developing high performance alloys

• Several options exist that may provide improved accident-tolerant fuel cladding for light water fission reactors compared to existing Zr alloy cladding