

Benchmarking the new ENDF/B-VIII.0 nuclear data library for OECD/NEA medium 1000 MWth sodium-cooled fast reactor

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Abstract. This paper presents the benchmark evaluation of the new ENDF/B-VIII.0 nuclear library for the OECD/NEA Medium 1000 MWth Sodium-cooled Fast Reactor (SFR). There are 2 SFR cores: metallic fueled (MET-1000) and oxide fueled (MOX-1000). The continuous-energy Monte Carlo Serpent2 code was used as the calculation tool. Various nuclear libraries such as ENDF/B-VII.1 and JENDL-4.0 were included to be compared with the newest ENDF/B-VIII.0. The evaluated parameters are k , β_{eff} , sodium void reactivity ($\Delta\rho_{Na}$), Doppler constant ($\Delta\rho_{Doppler}$), and control rod worth ($\Delta\rho_{CR}$).

1 Introduction

Under the working party of OECD/NEA (Organisation for Economic Co-operation and Development/Nuclear Energy Agency), the neutronics benchmark study of the Generation-IV sodium-cooled fast reactor (SFR) concepts has been performed and published using different methods and codes [1–3] in conjunction with various nuclear data libraries such as ENDF/B-VII.0 [4], ENDF/B-VII.1 [5], JEFF-3.1 [6], and JENDL-4.0 [7]. The benchmark consists of large 3600MWth carbide and oxide cores, and also medium 1000 MWth metallic and oxide cores. In this paper, the medium SFR cores are calculated by using the new version of nuclear data library, ENDF/B-VIII.0 [8], which has been released in 2018. The newer library has improvement on many neutron cross section libraries including the cross sections of materials which are commonly used in the SFR such U-235 and Pu-239 in the fuel, Fe-56 in the clad, and O-16 for mixed oxide fuel.

Since accuracy of the nuclear data is very important for the design and safety of a nuclear reactor, the impact of the new ENDF/B-VIII.0 on the neutronics and kinetics parameters of the OECD/NEA Medium 1000 MWth SFR is investigated. Both metallic and oxide cores are considered to distinguish the impact of the neutron spectrum. Several important neutronics parameters are evaluated such as effective neutron multiplication factor k , total effective delayed neutron fraction β_{eff} , prompt neutron generation time Λ , Doppler constant K_D , coolant void reactivity (CVR), and control rod (CR) worth. Each parameter is calculated at beginning of cycle (BOC) and end of cycle (EOC) using the continuous-energy Monte Carlo Serpent2 code [9]. Three different modern nuclear data libraries are considered which are ENDF/B-VIII.0, ENDF/B-VII.1,

and JENDL-4.0. Beside inter-library comparison, the calculated results are also compared to the result reported by the working group [3]. It should be noted that the reported result is an average result computed by different calculation methods and various nuclear data libraries.

2 Core Description

The layout of the metallic core is illustrated in Fig. 1. The core consists of inner and outer fuel regions, surrounded by reflector and shielding. Inner core region has 78 fuel sub-assemblies and outer core region has 102 fuel sub-assemblies. Meanwhile, there are 114 reflector sub-assemblies, 66 shielding sub-assemblies, 15 primary control sub-assemblies, and 4 secondary control sub-assemblies.

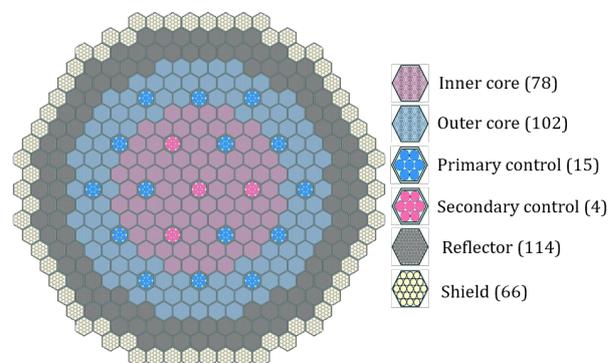


Figure 1. Radial Layout of Metallic Core [1]

The fuel consists of irradiated U-10Zr metallic fuel and it is contained in HT-9 cladding. The total core height is 480.20, while the active core height is about 85.82 cm.

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In the calculation, the temperature of the fuel is 534°C, and the temperature of coolant and structural material is 432.5°C.

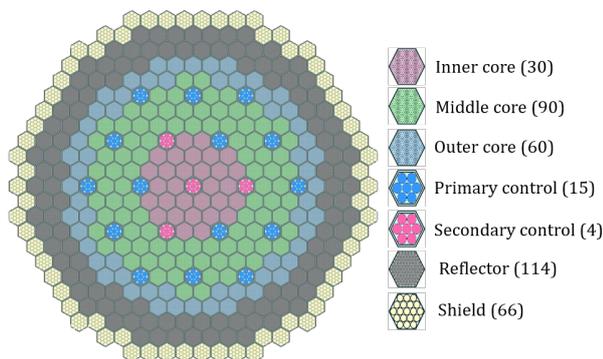


Figure 2. Radial Layout of Oxide Core [1]

In Fig. 2, the radial layout of the oxide core is shown. The core has 3 fuel regions which are inner, mid, and outer regions. The fuel is irradiated $\text{UO}_2\text{-(TRU)-O}_2$ contained in HT-9 clad. There are 30 inner fuel sub-assemblies, 90 mid fuel sub-assemblies, and 60 outer fuel sub-assemblies. Meanwhile the number of non-fuel sub-assemblies is same as in the metallic core. The total core height is also same as in the metallic core, however the active core is slightly taller, about 114.94 cm. The fuel temperature is also higher, about 1027°C, and the other components have same temperatures as in metallic core. For detail information on the benchmark including the material compositions and assembly dimension, one can refer to [1].

3 Results and Discussion

The Monte Carlo Serpent2 code was used to produce the subsequent results. In the calculation, the sub-assembly in the core was explicitly modeled. Each calculation used 100,000 neutron histories and 1,050 total neutron cycles with 50 inactive ones. Using this calculation condition, the standard deviation of k is about 7 pcm.

The effective neutron multiplication factor k values for metallic and oxide cores are summarized in Tables 1 and 2, respectively. Comparing among the different libraries, JENDL-4.0 provides the highest k value of the metallic core at BOC and EOC than the ones by ENDF/B-VII.0 and ENDF/B-VII.1. Meanwhile, both JENDL-4.0 and ENDF/B-VII.1 produce similar k and they are higher than the one by ENDF/VIII.0 for oxide core. It is noted that the calculated k values are lower than the ones reported [3]. Additional analysis to evaluate the impact of ENDF/B-VIII.0 library was also conducted by replacing a single isotope from the old library by a new one from ENDF/B-VIII.0 library at BOC, summarized in Tables 3 and 4. It is noticed that there is significant k changes from Fe-56 and U-238 of ENDF/B-VII.1 and Fe-56 and Pu-239 of JENDL-4.0 for both cores.

Figures 3 and 4 show the sensitivity coefficient of k for metallic and oxide cores respectively. The sensitivity

Table 1. k of metallic core at BOC and EOC

Library	BOC	EOC
ENDF/B-8.0	1.02993 ± 0.00007	1.00580 ± 0.00007
ENDF/B-7.1	1.02808 ± 0.00007	1.00522 ± 0.00007
JENDL-4.0	1.03240 ± 0.00007	1.00893 ± 0.00007
Reported [3]	1.03578 ± 0.0078	1.01280 ± 0.0071

Table 2. k of oxide core at BOC and EOC

Library	BOC	EOC
ENDF/B-8.0	1.02362±0.00006	1.00567±0.00006
ENDF/B-7.1	1.02610±0.00006	1.00857±0.00006
JENDL-4.0	1.02539±0.00006	1.00876±0.00007
Reported [3]	1.02860±0.0062	1.01360±0.0082

Table 3. Impact of the specific isotope library from ENDF/B-VIII.0 to k of metallic core at BOC

Old Library	Library from ENDF/B-8.0	Change [pcm]
ENDF/B-7.1	Na-23	14 ± 7
	Fe-56	-466 ± 7
	U-235	6 ± 7
	U-238	266 ± 7
	Pu-239	86 ± 7
JENDL-4.0	Am-241	8 ± 7
	Na-23	68 ± 7
	Fe-56	-281 ± 7
	U-235	15 ± 7
	U-238	32 ± 7
	Pu-239	-145 ± 7
	Am-241	-94 ± 7

Table 4. Impact of the specific isotope library from ENDF/B-VIII.0 to k of oxide core at BOC

Old Library	Library from ENDF/B-8.0	Change [pcm]
ENDF/B-7.1	O-16	-33 ± 9
	Na-23	-8 ± 9
	Fe-56	-569 ± 9
	U-235	-14 ± 9
	U-238	205 ± 9
JENDL-4.0	Pu-239	-42 ± 9
	Am-241	-10 ± 9
	O-16	16 ± 9
	Na-23	96 ± 9
	Fe-56	-348 ± 9
	U-235	13 ± 9
	U-238	78 ± 9
	Pu-239	-288 ± 9
	Am-241	-65 ± 9

coefficients are consistent among different nuclear data libraries. It is noticed that Pu-239 (n,f), U-238 (n,f), Pu-240 (n,f), and Pu-241 (n,f) give the large positive sensitivities for both cores. Meanwhile, U-238 (n,g) and (n,inl) dominate the negative sensitivities for metallic core. On the other hand, the large negative sensitivities for oxide core include U-238 (n,g) and (n,inl), Pu-239 (n,g), O-16 (n,el), Pu-240 (n,g), and Fe-56 (n,inl).

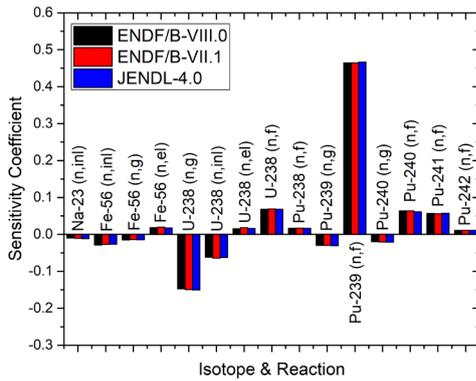


Figure 3. Sensitivity coefficient of metallic core for different nuclear data libraries

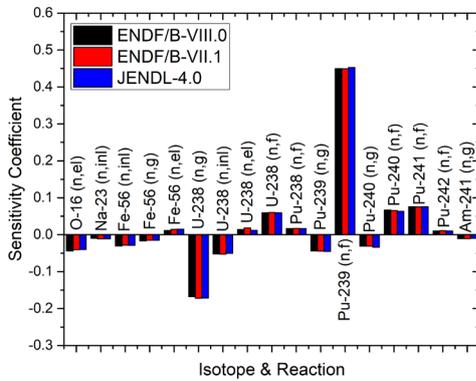


Figure 4. Sensitivity coefficient of oxide core for different nuclear data libraries

The calculated kinetic parameters Λ and β_{eff} at BOC and EOC are shown in Figs. 5 and 6 respectively. The parameters are adjoint-weighted value, calculated using the infinite fission probability method implemented in Serpent2. The Λ of metallic core is shorter than the one of oxide core due to the harder spectrum in the metallic core, while the β_{eff} of the metallic core is higher than the one of oxide core due to less amount of Pu and minor actinide in the metallic core. It is noted that the three different libraries produce similar and consistent kinetic parameters. Meanwhile, the reported β_{eff} [3] is slightly higher than the calculated values.

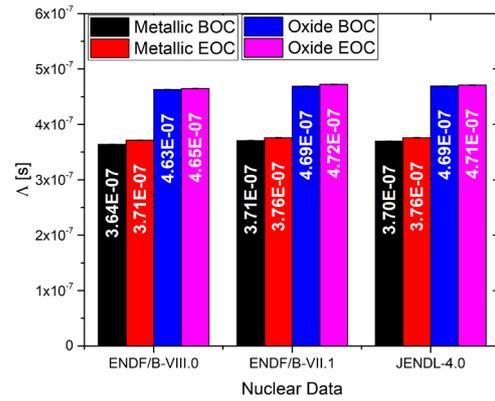


Figure 5. Λ of both cores for different nuclear data libraries

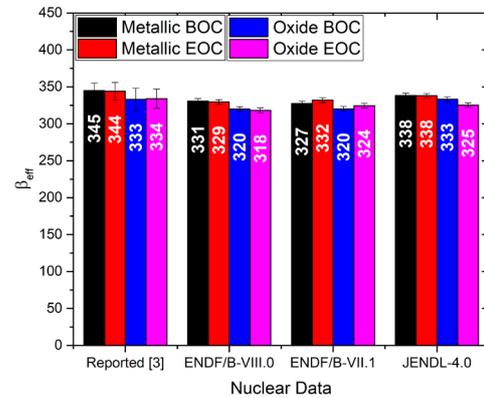


Figure 6. β_{eff} of both cores for different nuclear data libraries

Figure 7 shows the Doppler constant K_D for both cores at BOC and EOC. It is defined as the reactivity difference when the fuel temperature is doubled and at normal fuel operating temperature. It is clearly shown that the oxide core has more negative K_D than the metallic core due to the softer spectrum in the oxide core. Moreover, the oxide core contains more U-238 than in metallic core. It is also noted that the similar and consistent K_D values are given by the three different libraries. Meanwhile, the reported K_D [3] is also slightly higher than the calculated ones.

The coolant void reactivity (CVR) is summarized in Figure 8 for both cores at BOC and EOC. It is defined as the reactivity difference when the coolant is voided and at normal condition. It is clearly shown that the metallic core has more positive (CVR) than the oxide core due to the harder spectrum in the metallic core. It is also noted that the similar and consistent CVR values are given by the three different libraries. Meanwhile, the reported CVR values [3] is lower than the calculated ones except for the oxide core by ENDF/B-VII.1.

The last result which is the control rod (CR) worth is shown in Fig. 9. It is calculated as the reactivity differ-

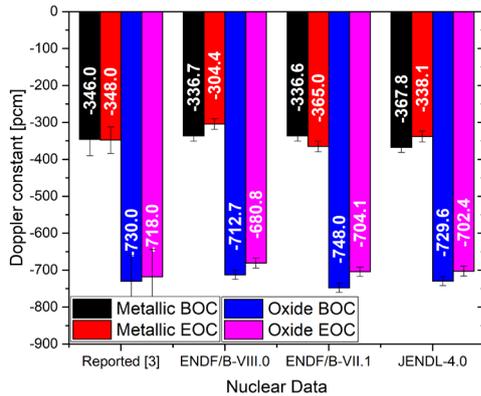


Figure 7. K_D of both cores for different nuclear data libraries

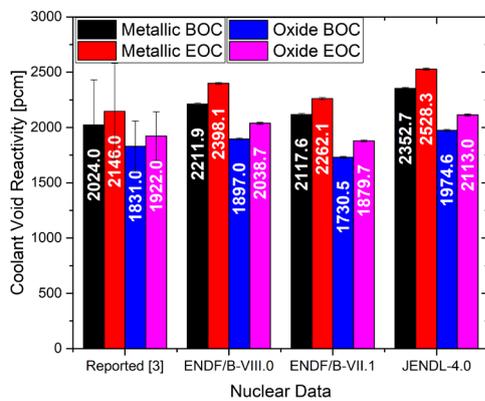


Figure 8. CVR of both cores for different nuclear data libraries

ence when all of the control sub-assemblies are withdrawn and inserted. It is also noted that the similar and consistent CR worth values are given by the three different libraries. Meanwhile, the reported CR worth values [3] is higher than the calculated ones.

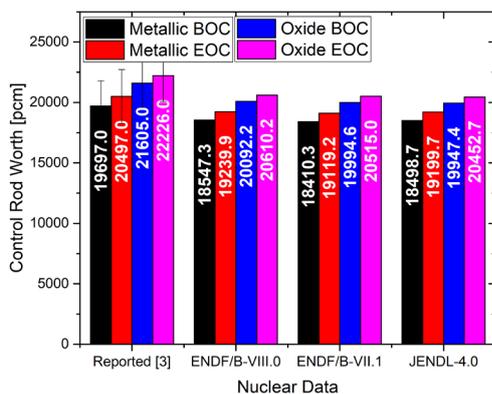


Figure 9. CR worth of both cores for different nuclear data libraries

4 Conclusion

Impact of the new released ENDF/B-VIII.0 nuclear data library to the neutronics and kinetics parameters of 2 different spectra SFR cores (metallic and oxide) has been studied. The new released Fe-56 cross section especially its (n, inl) and (n, g) cross sections shows significant reduction on k compared to the ones with ENDF/B-VII.1 and JENDL-4.0. Another significant impact includes the U-238 of ENDF/B-VII.1 and Pu-239 of JENDL-4.0. On the other hand, the values of kinetics parameters, Doppler constant, coolant void reactivity, and control rod worth between libraries are consistent.

References

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