

# On-the-fly temperature-dependent cross section treatment under extremes in RMC code

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**Abstract.** Neutron transport relevant to inertial confinement fusion always involves extremes, in which the physical quantities are extremely high, widely distributed and changes rapidly with space and time. In order to solve the memory and efficiency problems in nuclear data storage and processing, the on-the-fly temperature-dependent cross section treatment technique was investigated and developed under extremes in RMC code. Different strategies were adopted for different energy regions, i.e., the free gas model in the thermal region, the TMS method with OK basis cross section temperature in the resolved resonance region, and the infinite dilution cross section in the unresolved resonance region, whereas the high energy region above the unresolved resonance region was not treated currently. The test results of Godiva sphere and plutonium sphere show that the on-the-fly technique has high accuracy, but the efficiency of the proposed technique still needs to be improved for some cases, and the optimization work with the elevated basis cross section temperatures is ongoing.

## 1 Introduction

Neutron transport relevant to inertial confinement fusion always involves extremes, in which the physical quantities are extremely high, widely distributed and changes rapidly with space and time. The temperature of the background material can be as high as 100-million Kelvin, and the maximum velocity of the boundary motion can reach 1 million meters per second. Moreover, both of the background temperature and the boundary motion velocity change rapidly with space and time in a wide range. Since the neutron cross section is a function of the neutron speed relative to the target nuclei, affected by the thermal motion of the target nuclei and the boundary motion, the traditional pre-generated cross section method [1] is invalid under extremes because of the memory limitation of computers. Trumbull [2] suggested that ACE dataset at every 10K could provide the accuracy need for simple interpolation between temperature points, considering the temperature range from room temperature to 100-million Kelvin, the amount of ACE data could reach about 11000TB, which is unacceptable for even super computers. Meanwhile, the generation of such large amount of dataset is very time consuming. In order to solve the memory and the efficiency problems in data storage and processing, the on-the-fly treatment of cross section is the right choice under extremes.

Since the consideration of the effect of both thermal motion and boundary motion on Doppler broadening is too complicated, this paper mainly focus on the temperature effect, the boundary motion effect will be taken into consideration in the future work. The on-the-fly temperature-dependent cross section treatment strategy in the continu-

ous energy Reactor Monte Carlo code RMC [3] was investigated and developed under extremes. Detailed description of the methods and the validation results are presented in the remainder part of this paper.

## 2 Methods

Neutron cross section as a function of the incident energy is generally divided into three regions in the conventional reactor physics, namely, the thermal region, the resonance region, and the high-energy region, while the resonance region could also be divided into resolved region and unresolved region, depending on the nuclide. Doppler broadening effect becomes pronounced with the increase of temperature, especially at high temperatures. The temperature effect on different energy regions show huge difference as shown in Fig. 1, which takes the total cross section of <sup>235</sup>U from ENDF/B-VIII.0 [4] library as an example. Therefore, different strategies are adopted for different energy regions.

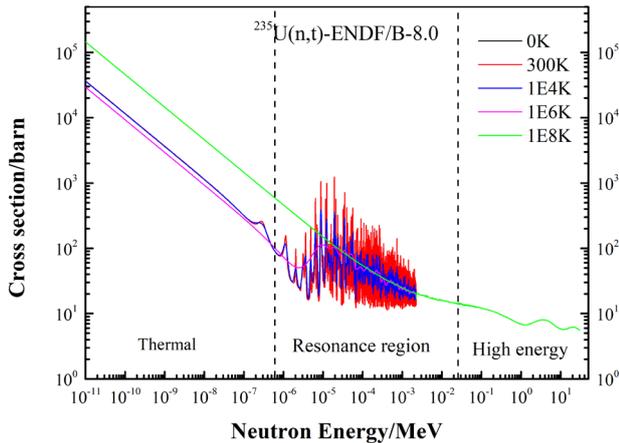
### 2.1 Thermal energy region

In the thermal energy region, since the number of neutrons is extremely small, the contribution of the thermal neutrons to the transport process is not as significant as that in the conventional reactor physics. In order to simulate the temperature effect accurately, the free gas model in RMC code is adopted to account for the temperature effect in the thermal region.

### 2.2 Resolved resonance region

In the resolved resonance region (RRR), where the temperature effect is very significant, two on-the-fly strate-

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**Figure 1.** Temperature effect on  $^{235}\text{U}$  total cross section from ENDF/B-VIII.0 library.

gies were developed in RMC code, the target motion sampling (TMS) [5] method and the improved Gauss-Hermite method [6]. Since the using of the Gauss-Hermite quadrature has limitation [7], the improved Gauss-Hermite method is invalid at high temperatures for some nuclides. While the TMS method takes the thermal motion of target nuclide into account explicitly. The coordinate transform to the target-at-rest frame at each collision site and the rejection sampling technique are used to model arbitrary temperatures with only 0K continuous-energy cross sections [5]. This method is a neutron tracking strategy with wide applicability at high temperatures, meanwhile, considering the combination with the boundary motion effect in the near future, TMS method is selected to handle the temperature effect in RRR, the details of this method can be referred to literatures [5, 8].

### 2.3 Unresolved resonance region and high energy region

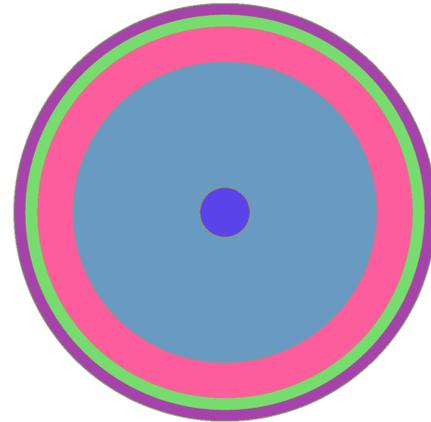
In the unresolved resonance region, since the resonance peak decreases significantly, the resonance self-screen effect will disappear at high temperatures [9], the infinite dilution cross section is adopted in this paper to simulate the temperature effect approximately. For the high energy region above the URR, the temperature effect was not treated currently.

## 3 Numerical results and analysis

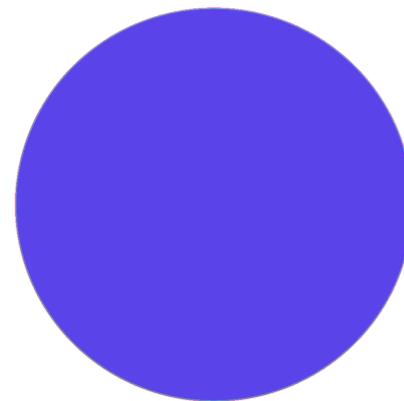
### 3.1 Test cases

Two cases of Godiva sphere and Plutonium sphere were modified and adopted to validate the on-the-fly technique under extremes. The Godiva sphere is a 10-layer-shell fast spectrum case, the central layer of the assembly is a high-enriched uranium (HEU) shell with an enrichment of about 93% for  $^{235}\text{U}$ , the middle part is a 4-layer HEU-polyethylene alternate shell, and the outer part is coated with HEU shell. The plutonium sphere is a 3-layer-shell

soft spectrum case, the central layer is a mixture of Plutonium, polyethylene, and iron, the middle layer is a stainless steel shell, and the outer layer is a thin cadmium coating. The sketches of the two cases plotted by RMC are given in Fig. 2 and Fig. 3.



**Figure 2.** Godiva sphere.



**Figure 3.** Plutonium sphere

In order to validate the accuracy of the on-the-fly strategy, two conditions were calculated, one is the 0K cross section with TMS method, the other is the accurate cross section temperature with Doppler-broadening rejection correction (DBRC) [5], which considers the temperature effect on both cross sections and energy direction distributions. The second condition is regarded as the reference. 0K ACE format neutron library data was taken from the ENDF/B-VII.0 [10] official site, and the accurate ACE format data at 300K, 1000K, 2000K, 5000K,  $10^4\text{K}$ ,  $10^5\text{K}$ ,  $10^6\text{K}$ ,  $10^7\text{K}$  were generated using the latest version of NJOY2016 [11] based on the ENDF/B-VII.0 neutron data library.

All the cases were calculated in the criticality mode using RMC code, version 2.5, for the Godiva sphere case, 30000 neutrons per cycle were used for total 150 cycles with 10 inactive cycles, and for the plutonium sphere case, 10000 neutrons per cycle were used for total 130 cycles

with 30 inactive cycles. All the calculations were conducted in the serial mode, using the intel (R) core(TM) i7-7700 CPU @3.60GHz processor.

### 3.2 Results and analysis

The fission rate as a function of the neutron energy for the two cases based on the accurate library with DBRC is given in Fig.4 and Fig.5. It can be observed that the neutrons with energy higher than 100keV contribute to the fission rate dominantly in the Godiva sphere. While in the plutonium sphere, neutrons in the energy range from 0.1eV to several keV contribute to the fission rate mostly, moreover, with the temperature increase, the energy of the mostly contributed neutrons increase simultaneously. These results also reveal that the temperature effect is pronounced for the soft energy spectrum and special attention needs to be paid under extremes.

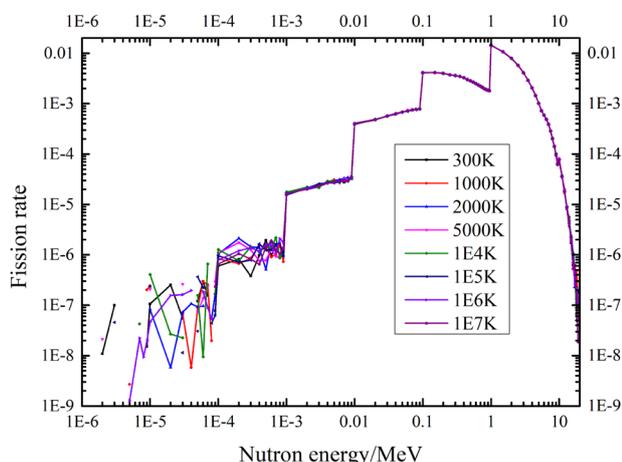


Figure 4. Fission rate distribution in Godiva sphere, layer 5.

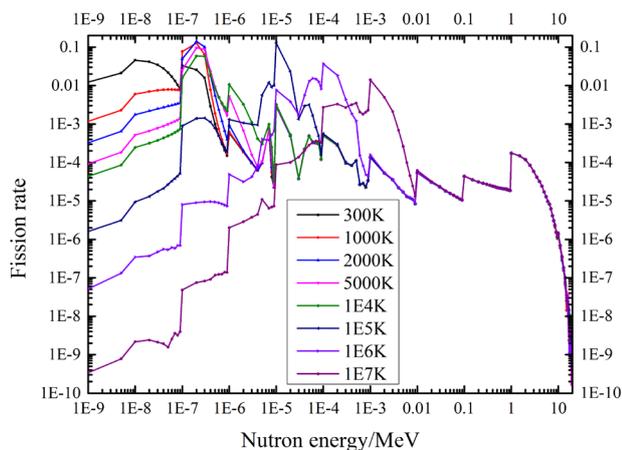


Figure 5. Fission rate distribution in Plutonium sphere.

The k-effective values, the standard deviation and the calculation time for the two cases are given in Table1 and Table2. In the comparison column, the  $\sigma$  is defined as  $\Delta k_{eff}$  divided by the  $k_{eff}$  of the reference (the accurate

library with DBRC), and  $\Delta k_{eff}$  is defined as the  $k_{eff}$  of the on-the-fly technique subtracted by that of the reference.

It can be found that the  $k_{eff}$  of the on-the-fly technique agrees with that of the reference within  $3\sigma$  (confidence level 99.73%) for both cases. For the fast spectrum Godiva case, the time consumption of the on-the-fly technique increase less than 50% compared to that of the standard method, while for the soft spectrum plutonium case, the time consumption increase with the temperature increase, at the temperature of  $10^7$ K, the time consumption increase about 30 times as that of the reference, which is unacceptable when applying the on-the-fly technique. Since this is the preliminary result, the optimization work with the elevated basis cross section temperatures is still ongoing, and will be reported in the near future.

### 4 Conclusion

The on-the-fly temperature-dependent cross section treatment technique under extremes in RMC code has been investigated and developed. The present work mainly focus on the temperature effect on neutron cross sections, and the boundary motion effect will be taken into consideration in the future work. Different strategies were adopted for different energy regions, i.e., the free gas model in the thermal region, the TMS method with OK basis cross section temperature in RRR, and the infinite dilution cross section in URR, whereas the high-energy region above the URR was not treated currently.

The test results of Godiva sphere and plutonium sphere show that the on-the-fly technique has high accuracy compared to the reference, while the efficiency of the proposed technique still needs to be improved for some cases, and the optimization work with the elevated basis cross section temperatures is ongoing.

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**Table 1.** Comparison of keff and time for the Godiva sphere

Temperature/K	Reference			On-the-fly			Comparison		
	$k_{eff}$	Std.	Time/min	$k_{eff}$	Std.	Time/min	$\Delta k_{eff}$	$\sigma$	Time ratio
300	1.000719	0.000289	0.6745	1.000723	0.000371	0.8563	-4E-06	-0.01384	1.27
1000	1.001121	0.00027	0.6713	1.000889	0.000376	0.8548	0.000232	0.859259	1.27
2000	1.00066	0.000305	0.6709	1.0004	0.000378	0.8721	0.00026	0.852459	1.30
5000	1.001587	0.000322	0.6680	1.001562	0.000383	0.8622	2.5E-05	0.07764	1.29
10 <sup>4</sup>	1.00069	0.000297	0.6682	1.000516	0.000337	0.8756	0.000174	0.585859	1.31
10 <sup>5</sup>	1.000079	0.000303	0.6632	1.000873	0.000366	0.8807	-0.00079	-2.62046	1.33
10 <sup>6</sup>	1.001402	0.000291	0.6681	1.000826	0.000381	0.9394	0.000576	1.979381	1.41
10 <sup>7</sup>	1.000797	0.000289	0.6927	1.000565	0.000359	1.0136	0.000232	0.802768	1.46

**Table 2.** Comparison of keff and time for the plutonium sphere

Temperature/K	Reference			On-the-fly			Comparison		
	$k_{eff}$	Std.	Time/min	$k_{eff}$	Std.	Time/min	$\Delta k_{eff}$	$\sigma$	Time ratio
300	0.989635	0.000713	1.4956	0.988625	0.001046	2.8652	-0.00101	-1.41655	1.91
1000	1.032701	0.000806	1.3337	1.031751	0.00088	2.5695	-0.00095	-1.17866	1.93
2000	1.02259	0.000756	1.3834	1.02028	0.000946	2.6427	-0.00231	-3.05556	1.91
5000	0.796182	0.000753	1.6717	0.794057	0.000791	3.7361	-0.00212	-2.82205	2.23
10 <sup>4</sup>	0.583257	0.000579	2.7292	0.581579	0.000815	5.7882	-0.00168	-2.8981	2.12
10 <sup>5</sup>	0.607844	0.000567	4.7721	0.608242	0.000844	14.5240	0.000398	0.70194	3.04
10 <sup>6</sup>	0.431459	0.000536	7.8892	0.431472	0.000798	49.8727	1.3E-05	0.024254	6.32
10 <sup>7</sup>	0.143356	0.000161	13.8834	0.143082	0.000319	416.676	-0.00027	-1.70186	30.01

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